

# COMPUTATIONAL STRUCTURAL MECHANICS AND DYNAMICS

MASTERS IN NUMERICAL METHODS

ASSIGNMENT 10

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## Solid and Structural Dynamics

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## 1 Problem 1

In the dynamic system of slide 6, let  $r(t)$  be a constant force  $F$ . What is the effect of  $F$  on the time-dependent displacement  $u(t)$  and the natural frequency of vibration of the system?

To solve for an undamped case we consider  $F = 0$

$$ku + m\ddot{u} = 0 \quad (1)$$

The equation of this system is given by  $u = u_0 \sin(\omega t + \phi)$ ,  $u_0$  being the amplitude, and  $\omega$  is the natural frequency of vibration, whose value is given by

$$\omega = \sqrt{\frac{k}{m}} \quad (2)$$

Now for the case of nonzero forces we can see that,

$$ku + m\ddot{u} = F \quad (3)$$

This is a non-homogeneous differential equation, the solution is given by

$$u(t) = u_c(t) + u_p(t) \quad (4)$$

Here,  $u_c$  is the complementary solution of the free undamped part, and  $u_p$  is the particular solution.

To solve the particular solution we solve

$$ku_p + m\ddot{u}_p = F \quad (5)$$

with  $u_p = c$  a constant

That gives us  $u_p = \frac{F}{k}$ , therefore we can say that

$$u(t) = \frac{F}{k} + u_0 \sin(\omega t + \phi) \quad (6)$$

The above equation shows that  $F$  does not affect the system as the particular solution which is dependent of  $F$  is independent of the frequency ( $\omega$ ). It is simply an offset value to the solution. The variation in  $F$  may change the value of  $u(t)$  but it will affect the displacement in the same way irrespective of the frequency.

## 2 Problem 2

A weight whose mass is  $m$  is placed at the middle of a uniform axial bar of length  $L$  that is clamped at both ends. The mass of the bar may be neglected. Estimate the natural frequency of vibration in terms of  $m$ ,  $L$ ,  $E$  and  $A$ .

The maximum displacement will be at  $x = \frac{L}{2}$  and it is given by

$$u_{max} = \frac{FL^3}{192EI} \quad (7)$$

If we consider a square beam, of side  $a$  we can write the moment of inertia as follows

$$I = \frac{bh^3}{12} = \frac{a^4}{12} \quad (8)$$

substituting in max displacement equation we get

$$u_{max} = \frac{FL^3}{16Ea^4} \quad (9)$$

Therefore the effective stiffness is

$$k = \frac{F}{\frac{FL^3}{16Ea^4}} = \frac{16Ea^4}{L^3} \quad (10)$$

The frequency is given by

$$\omega = \sqrt{\frac{k}{m}} = \sqrt{\frac{16Ea^4}{mL^3}} = \frac{4a^2}{L} \sqrt{\frac{E}{mL}} \quad (11)$$

### 3 Problem 3

Use the expression on slide 18 to derive the mass matrix of slide 17.

The expression is

$$\mathbf{m} = \int \mathbf{N}^T \mathbf{N} \rho dV \quad (12)$$

We can write this as

$$m_{ij} = \rho AL \int_0^1 N_i N_j d\eta \quad (13)$$

Now we can introduce shape functions for this problem  $N_1 = 1 - \eta$  and  $N_2 = \eta$ .

The equation becomes

$$\mathbf{M} = \rho AL \int_0^1 \begin{bmatrix} N_1^2 & N_1 N_2 \\ N_1 N_2 & N_2^2 \end{bmatrix} d\eta \quad (14)$$

Now we can calculate these individually, as following

$$\int_0^1 N_1^2 d\eta = \int_0^1 (1 - 2\eta + \eta^2) d\eta = \frac{1}{3} \quad (15)$$

$$\int_0^1 N_1 N_2 d\eta = \int_0^1 (\eta - \eta^2) d\eta = \frac{1}{6} \quad (16)$$

$$\int_0^1 N_2^2 d\eta = \int_0^1 (\eta^2) d\eta = \frac{1}{3} \quad (17)$$

The final mass matrix turns out to be

$$\mathbf{M} = \frac{\rho AL}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix} \quad (18)$$

## 4 Problem 4

**Obtain also the mass matrix of a two-node, linear displacement element with a variable cross-sectional area that varies from  $A_1$  to  $A_2$ .**

The variation in the area can be defined as follows

$$A(\eta) = \sum N_i(\eta)A_i \quad (19)$$

The shape functions for a linear iso-parametric element are given by  $N_1 = \frac{1}{2}(1 - \eta)$  and  $N_2 = \frac{1}{2}(1 + \eta)$

Therefore the mass matrix is given by the following expression,

$$\mathbf{M} = \int_{-1}^1 \begin{bmatrix} \frac{1}{2}(1 - \eta) \\ \frac{1}{2}(1 + \eta) \end{bmatrix} \begin{bmatrix} \frac{1}{2}(1 - \eta) & \frac{1}{2}(1 + \eta) \end{bmatrix} \rho \left( \frac{A_1}{2}(1 - \eta) + \frac{A_2}{2}(1 + \eta) \right) |J| d\eta \quad (20)$$

The Jacobian  $|J| = \frac{L}{2}$ , Further simplifying 20 we get

$$\mathbf{M} = \int_{-1}^1 A_1 \begin{bmatrix} -(\eta - 1)^3 & (\eta - 1)^2(\eta + 1) \\ (\eta - 1)^2(\eta + 1) & (\eta + 1)^2(\eta - 1) \end{bmatrix} + A_2 \begin{bmatrix} (\eta - 1)^2(\eta + 1) & -(\eta + 1)^2(\eta - 1) \\ -(\eta + 1)^2(\eta - 1) & (\eta + 1)^3 \end{bmatrix} d\eta \quad (21)$$

Finally performing the integration in the given limits we obtain

$$\mathbf{M} = \frac{\rho L}{12} \begin{bmatrix} 3A_1 + A_2 & A_1 + A_2 \\ A_1 + A_2 & A_1 + 3A_2 \end{bmatrix} \quad (22)$$

