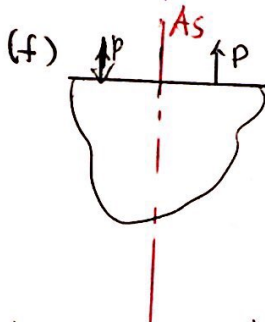
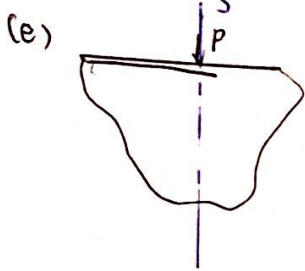
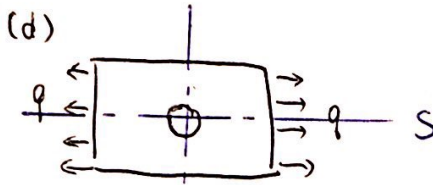
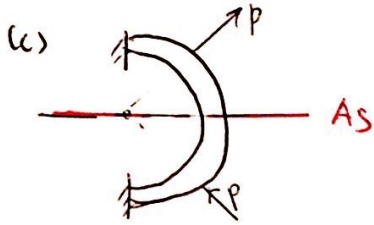
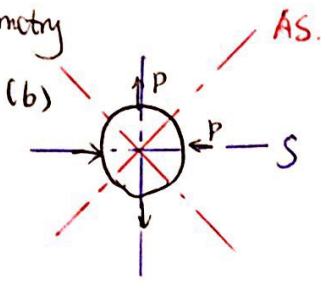
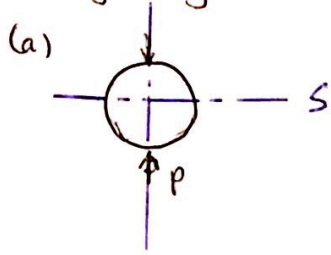
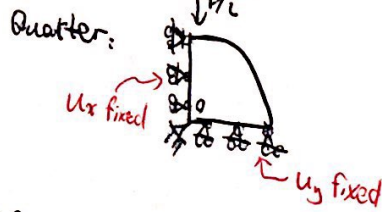
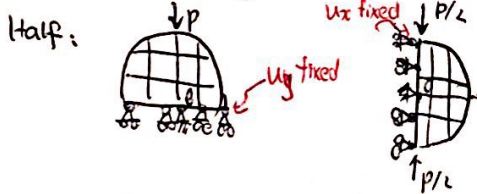


2.1 FEM Modelling.

1. S: Symmetry AS: Antisymmetry

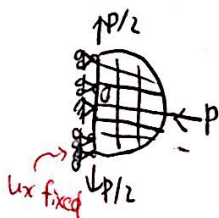
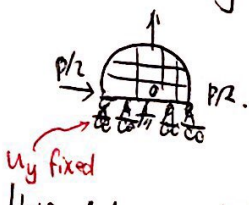


2. (a) We can cut the complete structure into one half or one quarter. The boundary conditions are applied so that there is no displacement perpendicular to the symmetry line. Node 0 is fixed to avoid free body motion.

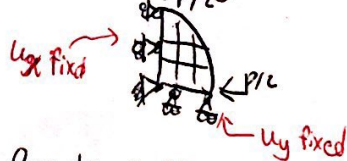


(b) The structure can be cut into half or quarter along the symmetry, antisymmetry line. Node 0 is fixed to avoid free body motion

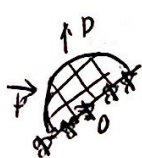
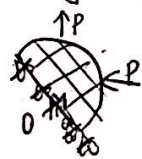
Half symmetry



Quarter symmetry



Half Antisymmetry

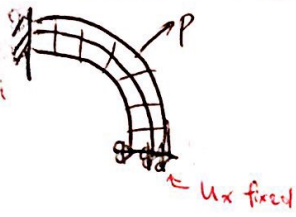


Quarter antisymmetry

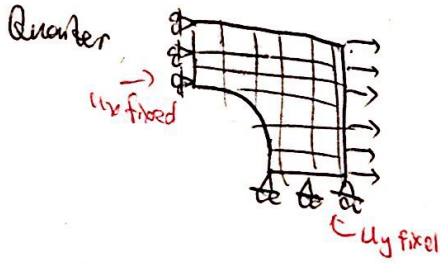
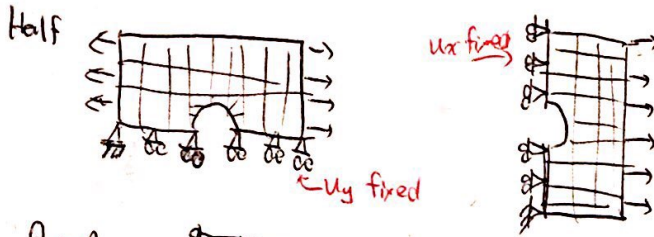


No displacement parallel to the antisymmetry line

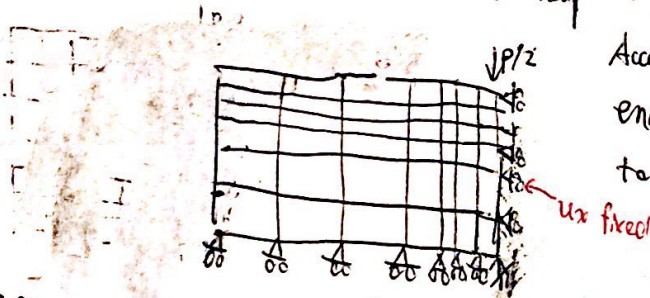
(c) The structure can be cut into half. No displacement parallel to the anti-symmetry line.



(d) The structure can be cut into half or quarter along the symmetry line.

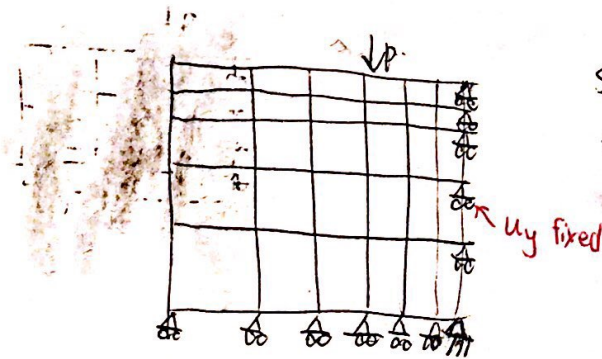


(e) The structure can be cut into half along the symmetry line



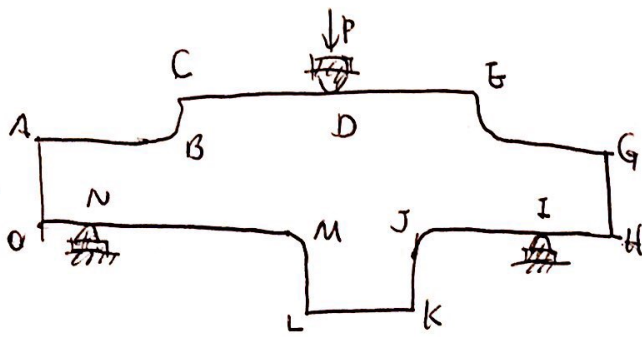
According to Saint-Venant's principle, if the half plate is large enough, the results from simulation will be similar to the analytical one

(f) The structure can be cut into half along the anti-symmetry line



Same reason as (e), when the plate is large enough, the results will be accurate

2.2



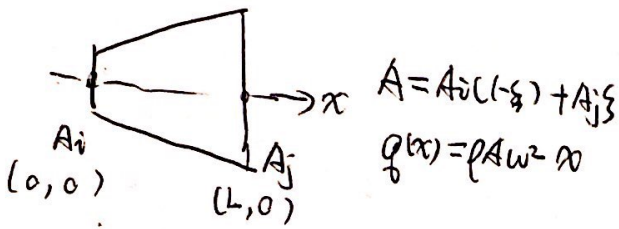
The trouble spots are

D: Vicinity of concentrated loads

B, M, J, F: abrupt corners,

N, I: vicinity of concentrated reactions

2.3 Variational Formulation



Natural coordinate $\xi = \frac{x}{L}$

The consistent force vector is calculated from

$$W^e = \int_0^L q u dx = \int_0^1 q N^T \underline{u}^e L d\xi = (\underline{u}^e)^T \int_0^1 q \begin{bmatrix} 1-\xi \\ \xi \end{bmatrix} L d\xi = (\underline{u}^e)^T \underline{f}^e \quad \underline{u}^e \text{ is arbitrary}$$

$$\underline{f}^e = \int_0^1 q \begin{bmatrix} 1-\xi \\ \xi \end{bmatrix} L d\xi$$

$$= \int_0^1 \rho A w^2 x \begin{bmatrix} 1-\xi \\ \xi \end{bmatrix} L d\xi$$

$$= \int_0^1 \rho A w^2 L^2 \xi \begin{bmatrix} 1-\xi \\ \xi \end{bmatrix} d\xi$$

$$= \rho w^2 L^2 \int_0^1 [A_i(1-\xi) + A_j \xi] \xi \begin{bmatrix} 1-\xi \\ \xi \end{bmatrix} d\xi$$

$$= \rho w^2 L^2 \begin{bmatrix} \frac{A_i}{2} + \frac{A_j}{3} \\ \frac{A_i}{3} + \frac{A_j}{2} \end{bmatrix}$$

If $A_i = A_j = A$, $\underline{f}^e = \rho w^2 L^2 \begin{bmatrix} \frac{A}{6} \\ \frac{A}{6} \end{bmatrix}$